

# Interfacial Phenomena in Metal-Slag Reactions: Past, Present and Future

M.A. Rhamdhani

Faculty of Engineering and Industrial Sciences  
Swinburne University of Technology

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# CONTENT



- > Introduction
  - Interfacial phenomena and its importance
- > Previous Studies on Interfacial Phenomena (Metal-Slag Reactions)
- > Challenges
- > Current Progress
- > Future Directions
- > Conclusions

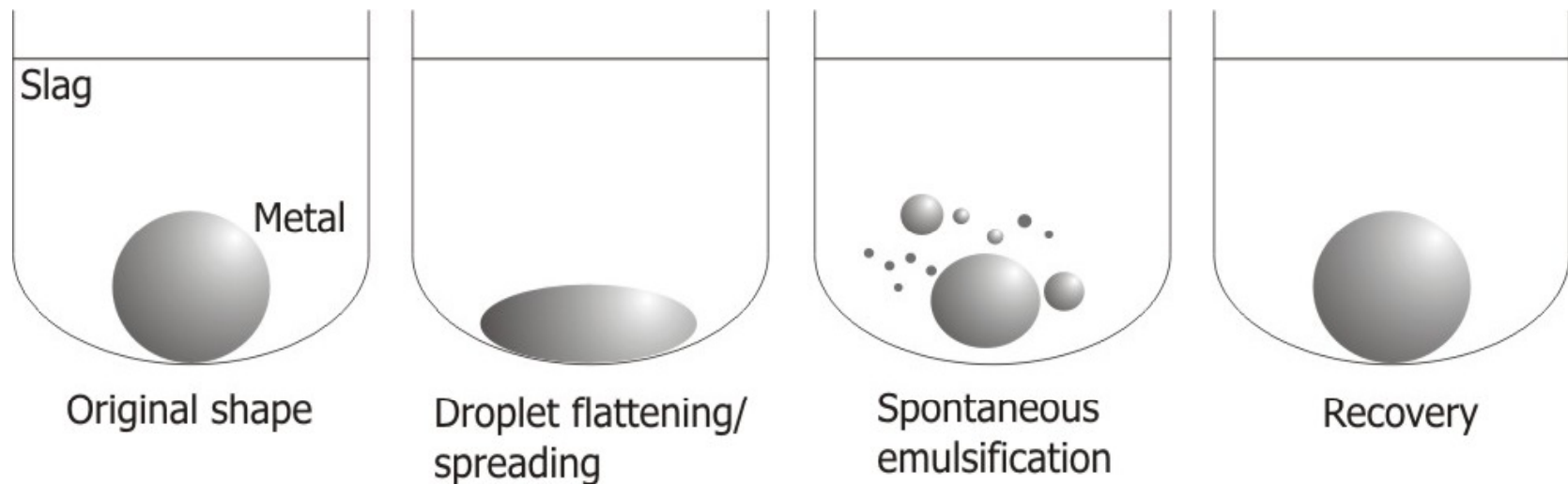
## INTRODUCTION



- > Dynamic interfacial phenomena?

“dynamic” → non-equilibrium

- > Behaviour of iron-alloy droplet reacting in liquid slag



Observed in

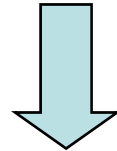
Liquid Fe-Al; Fe-C-S; Fe-Ti; Fe-P; Fe-B; Fe-Cr; Fe-Si alloys reacting in liquid slag

# INTRODUCTION

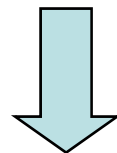


## DYNAMIC INTERFACIAL PHENOMENA:

Spontaneous emulsification, Surface roughening, Droplet flattening

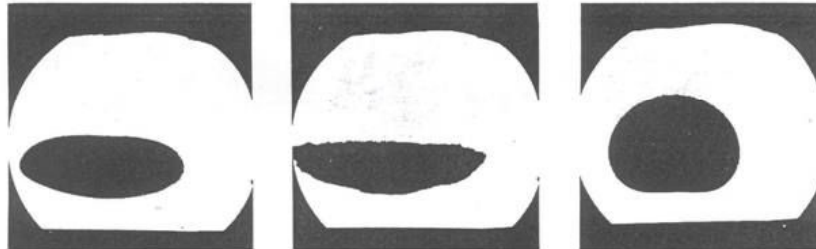


- Spontaneous increase of reacting interface area
- Enhancement of mass transport (several orders)
  - Increase in global kinetics



Speed up the processing time

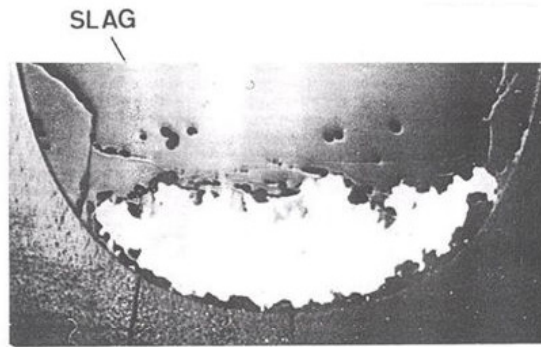
# PREVIOUS STUDIES IN INTERFACIAL PHENOMENA



(a)

(b)

(c)

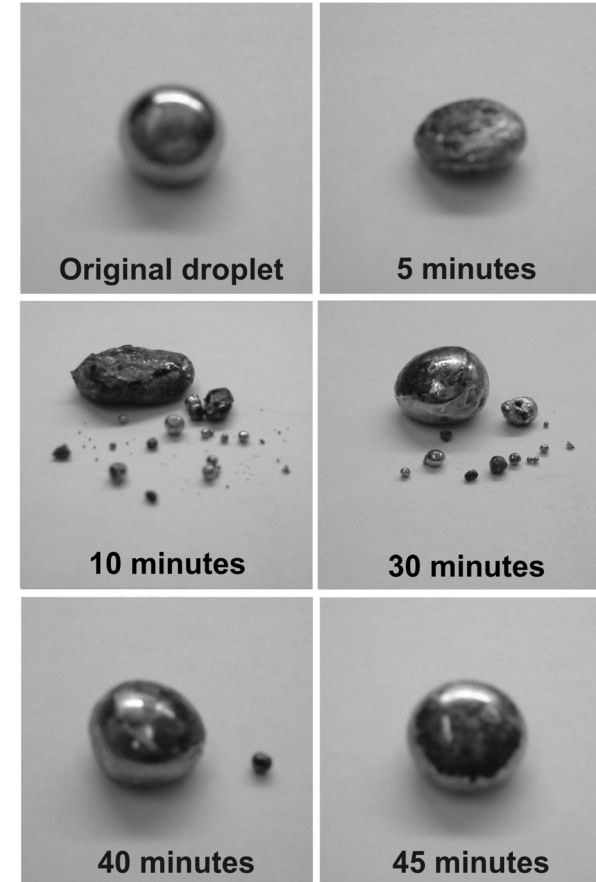


(d)

2.5g Fe-4.45%Al at 1600°C

(a) 7 min; (b) 18 min; (c) 40 min;

(d) polished section of b,  
from Riboud and Lucas (1981)



Original droplet

5 minutes

10 minutes

30 minutes

40 minutes

45 minutes

2.35g Fe-4%Al droplet in  
CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> slag at 1650°C,  
from Rhamdhani et al (2004)

# PREVIOUS STUDIES IN INTERFACIAL PHENOMENA

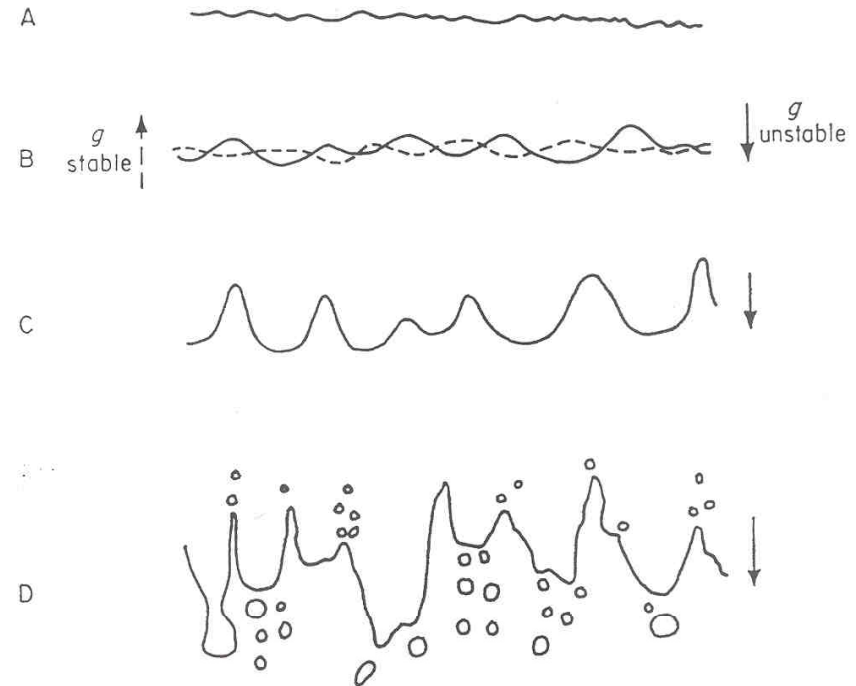
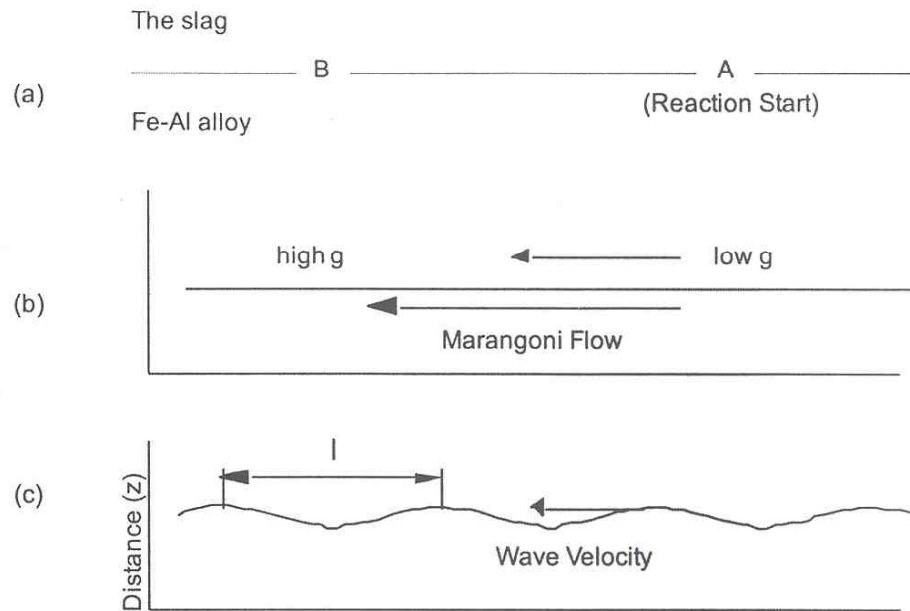
Researcher	Details										
Kozakevitch <i>et al.</i> (1955)	<ul style="list-style-type: none"> <li>• Fe-C-S droplets + CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> slag</li> <li>• Utilized x-ray</li> </ul>										
Deryabin <i>et al.</i> (1968) & Saburov <i>et al.</i> (1971)	<ul style="list-style-type: none"> <li>• Fe-S and Fe-C-S + CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> slag at 1450°C and 1550°C</li> <li>• Fe-Ti droplets (10 - 20wt% of Ti) with the same slag at 1540°C and 1580°C</li> <li>• Fe-Al (5, 10 and 20wt% Al) + CaO-Al<sub>2</sub>O<sub>3</sub>-TiO<sub>2</sub> slag</li> <li>• Utilized x-ray</li> </ul>										
Ooi <i>et al.</i> (1974)	<p>Observed the phenomena in:</p> <ul style="list-style-type: none"> <li>• Fe-Al and Fe-Ti + CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> (40:40:20 in wt%) slag at 1570°C</li> <li>• Kinetic study assuming constant interfacial area</li> <li>• Utilized x-ray</li> </ul>										
Riboud and Lucas (1981)	<ul style="list-style-type: none"> <li>• Various metal-slag systems; using x-ray</li> </ul> <table style="width: 100%; border: none;"> <tr> <td style="width: 50%;">Fe-Al + CaO-SiO<sub>2</sub> (or -Al<sub>2</sub>O<sub>3</sub>)</td> <td style="width: 50%;">Fe-Al + CaO-Al<sub>2</sub>O<sub>3</sub>-Fe<sub>2</sub>O<sub>3</sub></td> </tr> <tr> <td>Fe-Si + Cu<sub>2</sub>O-Al<sub>2</sub>O<sub>3</sub></td> <td>Fe-C-S + CaO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub></td> </tr> <tr> <td>Fe-Ti + CaO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub></td> <td>Fe-P + CaO-Al<sub>2</sub>O<sub>3</sub>-Fe<sub>2</sub>O<sub>3</sub></td> </tr> <tr> <td>Fe-B + CaO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub>-Fe<sub>2</sub>O<sub>3</sub></td> <td>Fe-Cr + CaO-SiO<sub>2</sub>-FeO</td> </tr> <tr> <td>Fe + Cu<sub>2</sub>O</td> <td></td> </tr> </table>	Fe-Al + CaO-SiO <sub>2</sub> (or -Al <sub>2</sub> O <sub>3</sub> )	Fe-Al + CaO-Al <sub>2</sub> O <sub>3</sub> -Fe <sub>2</sub> O <sub>3</sub>	Fe-Si + Cu <sub>2</sub> O-Al <sub>2</sub> O <sub>3</sub>	Fe-C-S + CaO-Al <sub>2</sub> O <sub>3</sub> -SiO <sub>2</sub>	Fe-Ti + CaO-Al <sub>2</sub> O <sub>3</sub> -SiO <sub>2</sub>	Fe-P + CaO-Al <sub>2</sub> O <sub>3</sub> -Fe <sub>2</sub> O <sub>3</sub>	Fe-B + CaO-Al <sub>2</sub> O <sub>3</sub> -SiO <sub>2</sub> -Fe <sub>2</sub> O <sub>3</sub>	Fe-Cr + CaO-SiO <sub>2</sub> -FeO	Fe + Cu <sub>2</sub> O	
Fe-Al + CaO-SiO <sub>2</sub> (or -Al <sub>2</sub> O <sub>3</sub> )	Fe-Al + CaO-Al <sub>2</sub> O <sub>3</sub> -Fe <sub>2</sub> O <sub>3</sub>										
Fe-Si + Cu <sub>2</sub> O-Al <sub>2</sub> O <sub>3</sub>	Fe-C-S + CaO-Al <sub>2</sub> O <sub>3</sub> -SiO <sub>2</sub>										
Fe-Ti + CaO-Al <sub>2</sub> O <sub>3</sub> -SiO <sub>2</sub>	Fe-P + CaO-Al <sub>2</sub> O <sub>3</sub> -Fe <sub>2</sub> O <sub>3</sub>										
Fe-B + CaO-Al <sub>2</sub> O <sub>3</sub> -SiO <sub>2</sub> -Fe <sub>2</sub> O <sub>3</sub>	Fe-Cr + CaO-SiO <sub>2</sub> -FeO										
Fe + Cu <sub>2</sub> O											

# PREVIOUS STUDIES IN INTERFACIAL PHENOMENA

Researcher	Details
Sharan and Cramb (1995)	<ul style="list-style-type: none"><li>• Utilized x-ray</li><li>• Fe-20Ni-2.39Al + CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> at 1550°C</li><li>• Proposed a mechanism for droplet flattening, i.e. due to difference of oxygen chemical potential</li></ul>
Chung and Cramb (1998, 2000)	<ul style="list-style-type: none"><li>• Utilized x-ray</li><li>• Optical and Scanning electron microscopy observation of the reacting interface</li><li>• Fe-Al + CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> and Fe-Ti + CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub></li><li>• Reported slag emulsification and evidence of non-uniform reaction</li><li>• Proposed a mechanism for spontaneous emulsification through Kelvin-Helmholtz instability</li></ul>

- Previous studies → phenomenological studies
- Lack of experimental data
- Holistic understanding of the phenomena is not yet achieved

# MECHANISM FOR THE PHENOMENA

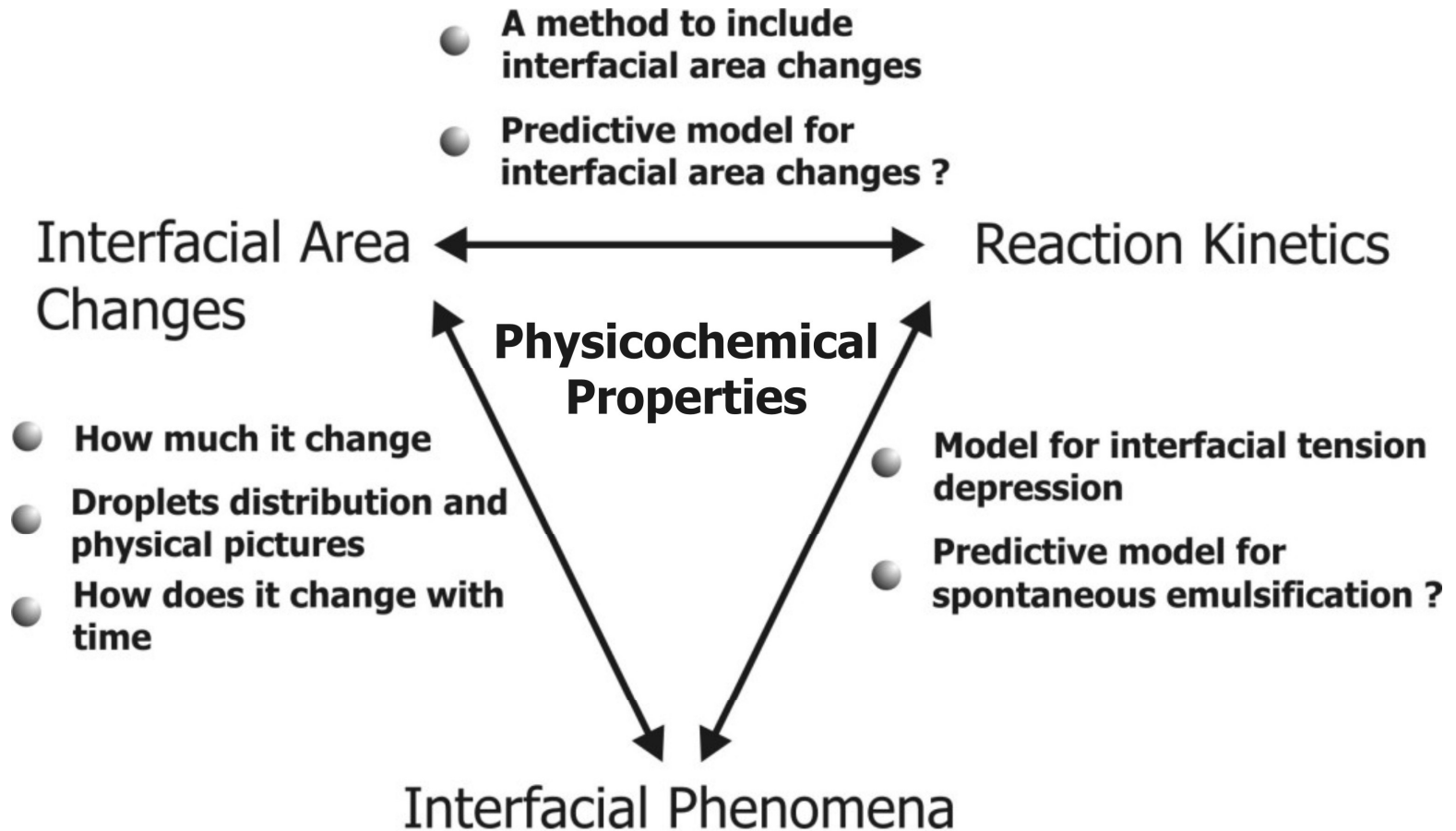


Marangoni flow leading to emulsification via Kelvin-Helmholtz instability (Chung & Cramb, 2000)

## Gradient of interfacial tension

- gradients of temperature (thermocapillarity)
- gradients of electrical potential (electrocapillarity)
- gradients of concentration (solutocapillarity)

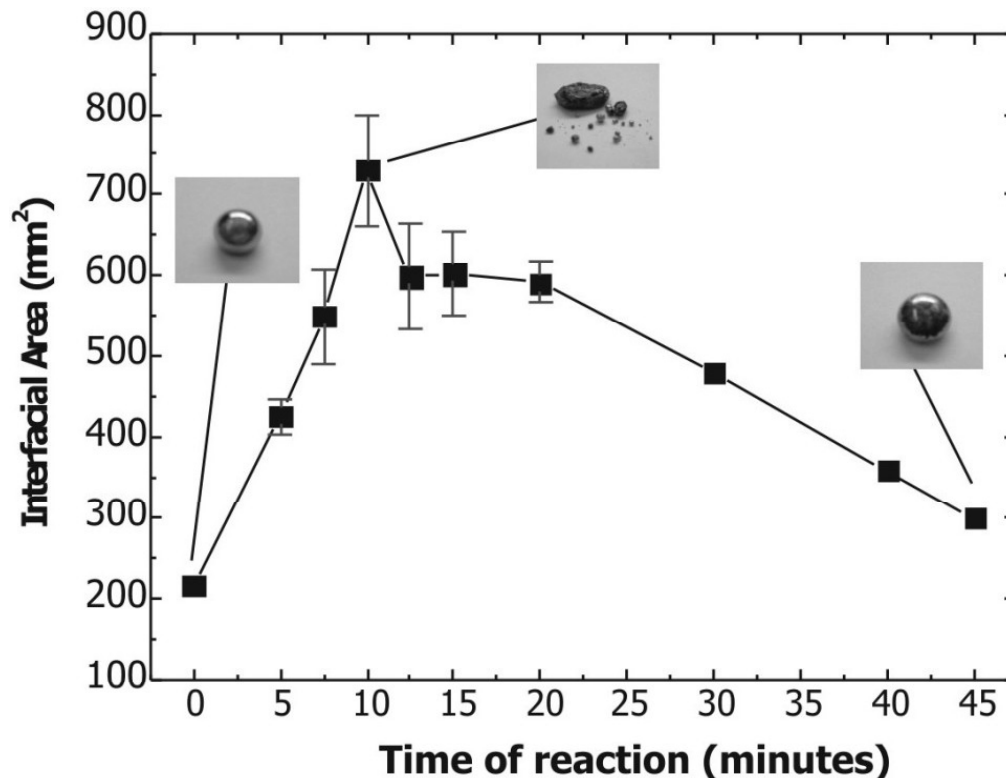
# CHALLENGES





## 1. Collection of interfacial area data during reaction

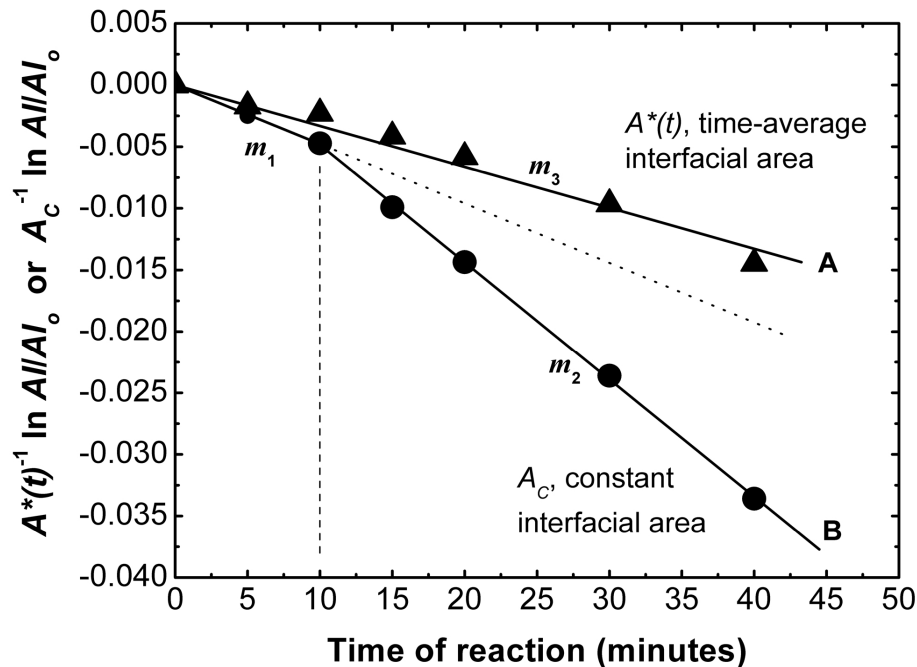
- Allows the development of the transient approach for kinetic analysis
- Interfacial area increase were found to be 300 to 500% (Rhamdhani *et al.*, 2005)



Fe-4%Al reacting in  
CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> at  
1650°C



## 2. Transient approach for kinetic analysis



> Mass transfer control in metal

$$\frac{V_m}{S} \frac{dC}{dt} = -k_m (C_b - C_i)$$

> Considering time-averaged interfacial area

$$\int_{\%Al_o}^{\%Al} \frac{d(\%Al)}{(\%Al)} = -\frac{k_m}{V_m} \int_0^t S(t) \cdot dt$$

$$\frac{1}{S^*(t)} \ln \frac{(\%Al)}{(\%Al)_o} = -\frac{k_m}{V_m} \cdot t$$

Considering time-averaged interfacial area



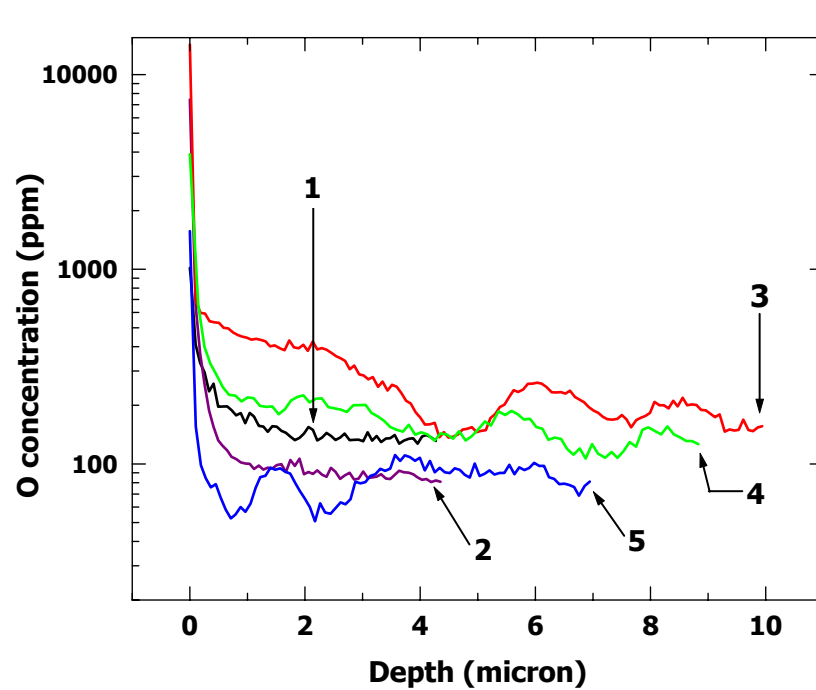
Fit in a single straight line

where

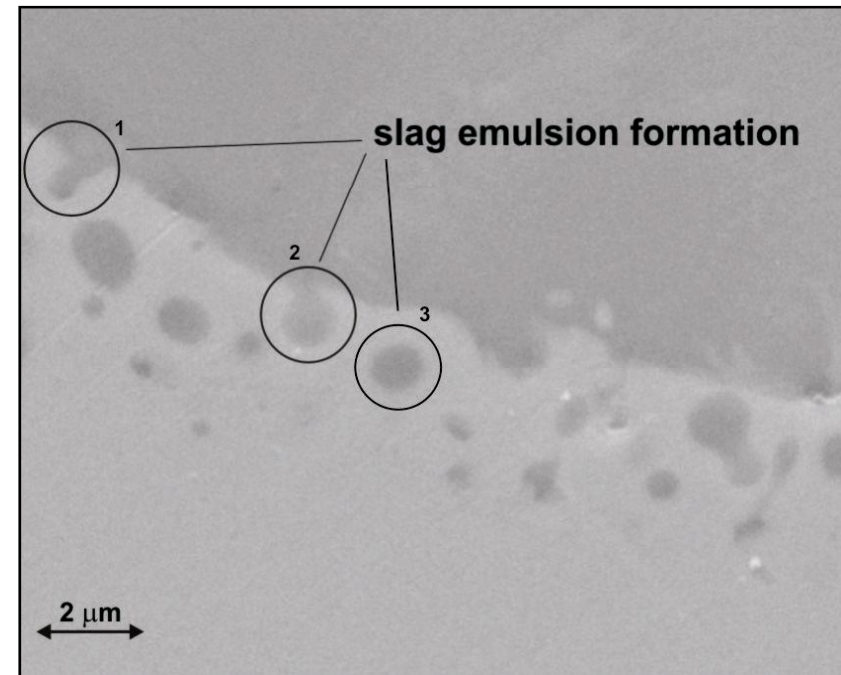
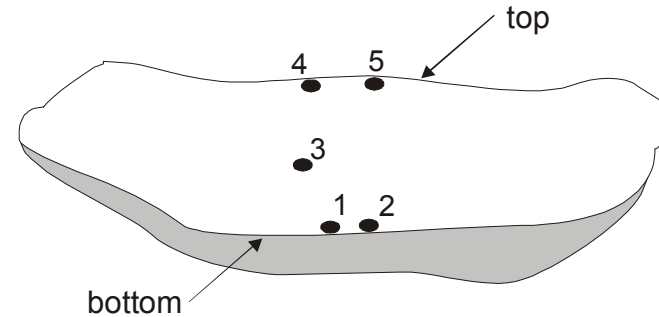
$$S^*(t) = \frac{1}{t} \cdot \int_0^t S(t) \cdot dt$$



**3. Interface characterization and solute oxygen analysis**

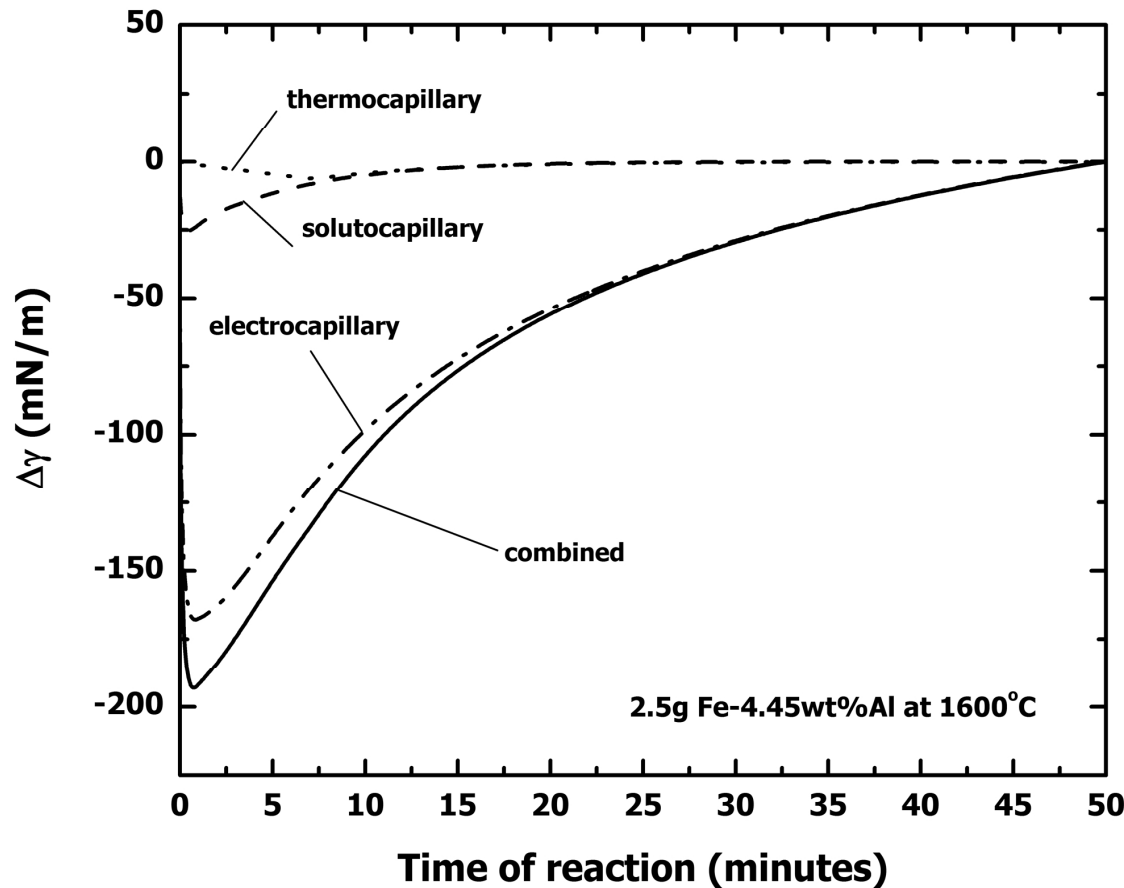


Dynamic SIMS Oxygen Depth Profile  
 Fe-4.45%Al + CaO-SiO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>  
 2.5g at 1600°C





4. Evaluation of the electro-, thermo- and solutocapillary effects



- > Adopting the local equilibrium concept and the utilization of the developed kinetic approach
  - Determination of local  $T$ ,  $\eta$ , and  $a_0$  (by using the kinetic information) and their contribution to the lowering of interfacial tension



- > Systematic experimental study to provide new data (interfacial tension, interfacial area, chemistry changes)
- > Development of predictive model for interfacial area changes
- > Understanding of the kinetics of electrochemical reactions and its relation to interfacial phenomena
- > Computational fluid modelling of interfacial instability and spontaneous emulsification



- > There are currently insufficient data to accurately determine the factors resulting the spontaneous emulsification
- > The studies up to date have provided a first base understanding of interfacial phenomena
- > Understanding the phenomena (including the ability to control them) is important for:
  - Improvement of existing technology → more energy efficient processes
  - Development of new processes

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Thank you for your attention!